Rhode Island Stormwater Design and Installations Standards Manual

Public Workshop
BMP Design - Critical
Elements
March 22, 2011

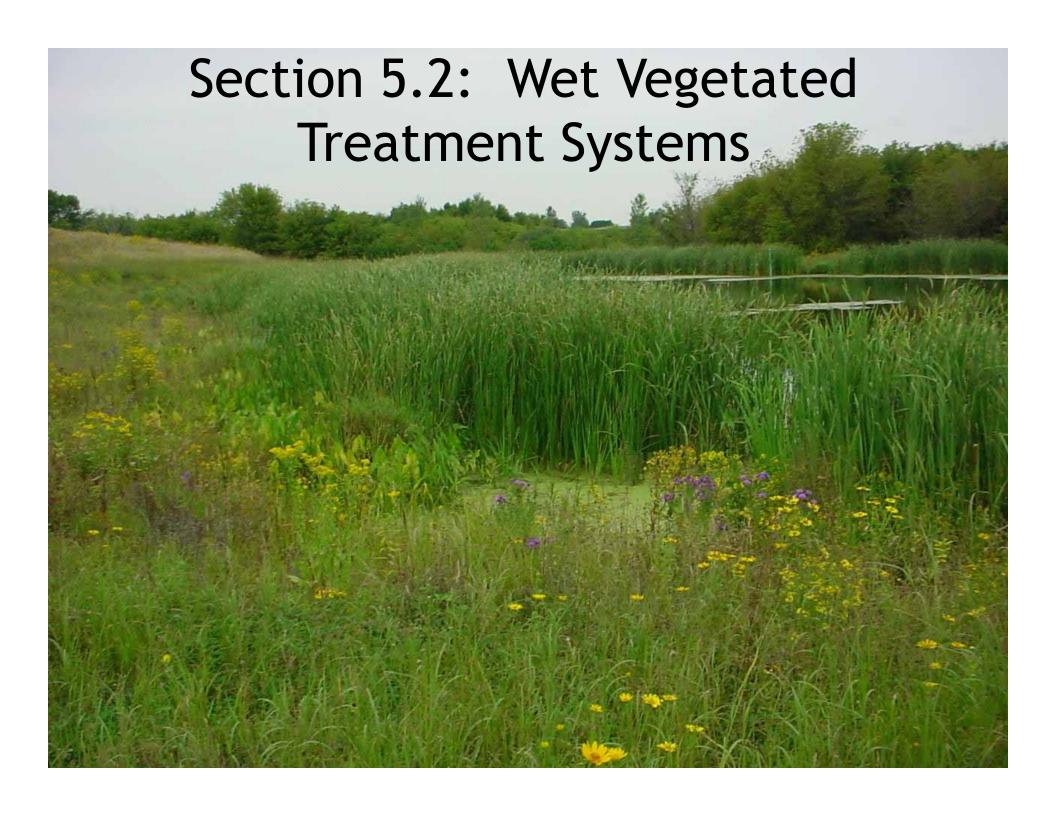
Presentation Outline

- Water Quality
- Pretreatment
- Storage

Minimum Design Criteria

- Required Elements and Design Guidance
 - If required elements can't be met, select a different BMP
- Six Categories
 - Feasibility
 - Conveyance
 - Pretreatment
 - Treatment
 - Landscaping
 - Maintenance





WVTS: Design Notes

- Shall not be located within jurisdictional waters, except may be allowed in previously developed upland buffers
- Restricted in cold-water fisheries watersheds
 - Discharges prohibited w/in 200 ft of jurisdictional waters
 - Beyond 200 ft, discharge up to the CP_v through an underdrained gravel trench outlet
- LUHPPL runoff requires a 3-ft separation to gw, no separation distance required for non-LUHPPL runoff
- Permanent pool volumes shall not be included in storage calcs for peak flow management (CP_{ν}/Q_{p})

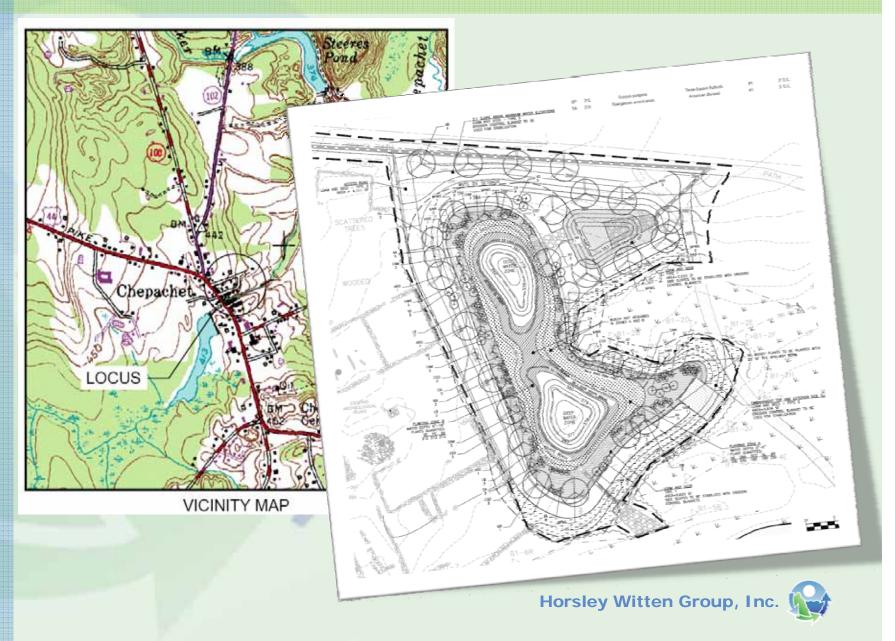
Shallow WVTS: Design Notes

- Min flowpath of 2:1 (length to width)
- High surface area to volume ratio
 - Pretreatment (10% of WQv)
 - Deepwater zones (25% of WQv)
 - Remaining 65% WQv combination of shallow pool and ED
- Shallow depths over most of surface area
 - 35% 6 inches or less
 - 65% 18 inches or less
- Complex internal microtopography, including aquatic benches
- Plant with emergent vegetation
- Consumes most land of any BMP
 - 1.5% of DA





Example - Chepachet, RI



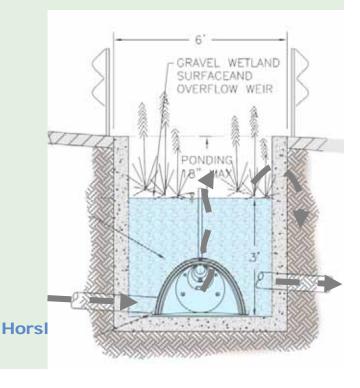
WET VEGETATED TREATMENT SYSTEM CALCULATIONS	REQUIRED	PROVIDED	UNITS
DRAINAGE AREAS AND WATER QUALITY VOLUME			
TOTAL CONTRIBUTING DRAINAGE AREA (10 Ac. MIN.)	n/a	439,520	sf
	n/a	10.1	acres
TOTAL IMPERVIOUS AREA (Tanyard/Oil Mill)	n/a	65,300	sf
	n/a	1.5	acres
TOTAL IMPERVIOUS AREA (RIDOT System Per Commonwealth)	n/a	190,800	sf
	n/a	4.4	acres
TOTAL IMPERVIOUS AREA	n/a	256,100	sf
	n/a	5.9	acres
RUNOFF DEPTH FOR WATER QUALITY VOLUME (WQv)	1.00	1.00	in
TREATMENT VOLUME REQUIRED (WQv)	0.49		ac-ft
	21,342		cf
PRETREATMENT			
SEDIMENT FOREBAY (10% OF WQv)	2,134	4,499	cf
	0.05	0.10	ac-ft

			u u
TREATMENT			
MIN. SURFACE AREA OF WVTS (1.5% of Drainage area)	6,593	9,570	sf
	0.15	0.22	acres
DEEPWATER ZONE VOLUME (25% of WQv)	5,335	5,988	cf
	0.12	0.14	ac-ft
HIGH MARSH AREA - 0"-6" DEPTH (35% of total surface area)	2,307	3,373	sf
	0.05	0.08	acres
TOTAL MARSH AREA - 0"-18" DEPTH (65% of Total Surface Area)	4,285	6,097	sf
	0.10	0.14	acres
GEOMETRY			
LENGTH	n/a	185	ft
WIDTH (average)	n/a	45	ft
WIDTH (maximum)	n/a	80	ft
RATIO (average)	2 to 1	4 to 1	L:W
RATIO (maximum)	2 to 1	2 to 1	L:W
CHANNEL PROTECTION VOLUME (CPv)			
RUNOFF VOLUME FROM 1-YR, 24-HR, TYPE III STORM (Vr)	n/a	17,860	cf
	n/a	0.41	ac-ft
CPv (0.65 x Vr)	11,609	13,565	cf
	0.27	0.31	ac-ft
LENGTH OF UNDERDRAINED GRAVEL TRENCH	35	36	lf

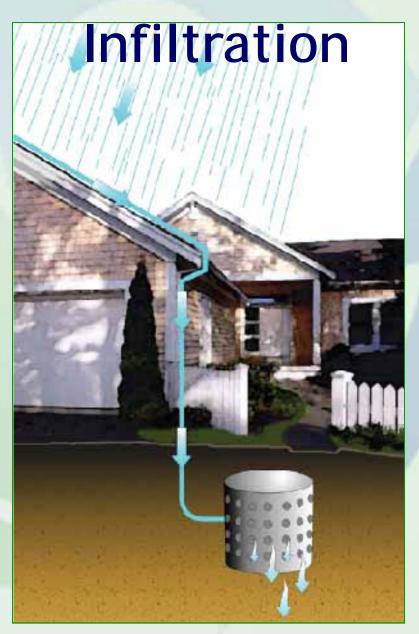
Gravel WVTS: Design Notes

- Min. length-to-width ratio 1:1, min. flowpath (L) of 15 ft
- Pretreatment: 10% WQv
- Remaining 90%, a combination of one or more basins/chambers filled with gravel and open ED
- Outlet invert just below gravel surface
- Surface area must be minimum 0.35% of DA
- May use organic soil
- Plant with emergent vegetation





Section 5.3:







Infiltration - Design Notes

- Field verification of soil permeability/texture essential
- Pretreatment essential minimum 25% of WQv
- Bottom of infiltration facility cannot be located in fill*, must have 3' separation from gw and bedrock*
- Size based on design infiltration rates (Table 5-3)
- Guidance: Keep drainage areas to each practice small, may reduce some potential problems
- * Reduced requirements for residential areas (2')

Table 5-3 Design Infiltration Rates for Different Soil Textures (Rawls et al., 1982)

	Design Infiltration	Design Infiltration
USDA Soil Texture	Rate (f _c) (in/hr)	Rate (f _c) (ft/min)
Sand	8.27	0.0115
Loamy Sand	2.41	0.0033
Sandy Loam	1.02	0.0014
Loam	0.52	0.0007
Silt Loam	0.27	0.0004

Design Notes (cont'd)

- Cannot be used if contributing drainage is a LUHPPL
- Higher maintenance burden
- Stabilize site prior to installation
- Must meet variety of setbacks* (Table 5-2)
- May be used for larger storm events if infiltration rate
 8.3 in/hr**, mounding analysis may be required

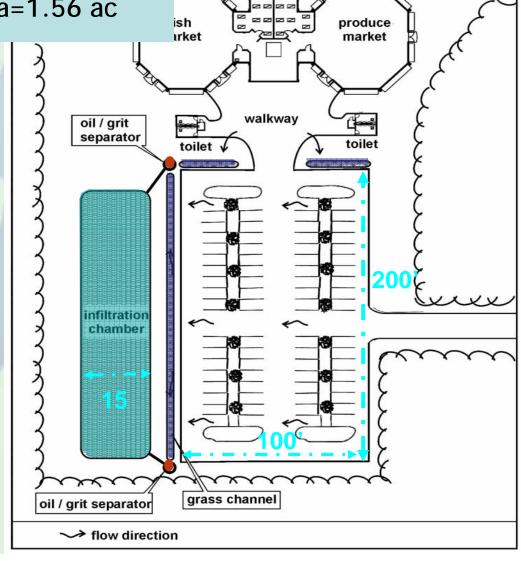
- * Reduced requirements for small-scale BMPs in res. areas
- ** 100% WQv treatment required by separate BMP in these areas



Sample Calculations

Total Disturbed Area = 3.0 ac Impervious Area=1.56 ac

The Sunshine Market is a hypothetical commercial development consisting of a fish and produce market. It is located in Charlestown, RI and discharges to Green Hill Pond. On-site soils are Windsor loamy sand (HSG "A").



preserve existing

vegetation as possible

Required Volume Calculations

•Compute required Re_v based on A soils and Sect 3.3.2

$$Re_v = [(1") (F) (I)] / 12$$

= $[(1") (0.6") (1.56 ac)] (1ft/12in)$
= $0.08 ac-ft = ~3,500 cf$

•Compute WQ_v

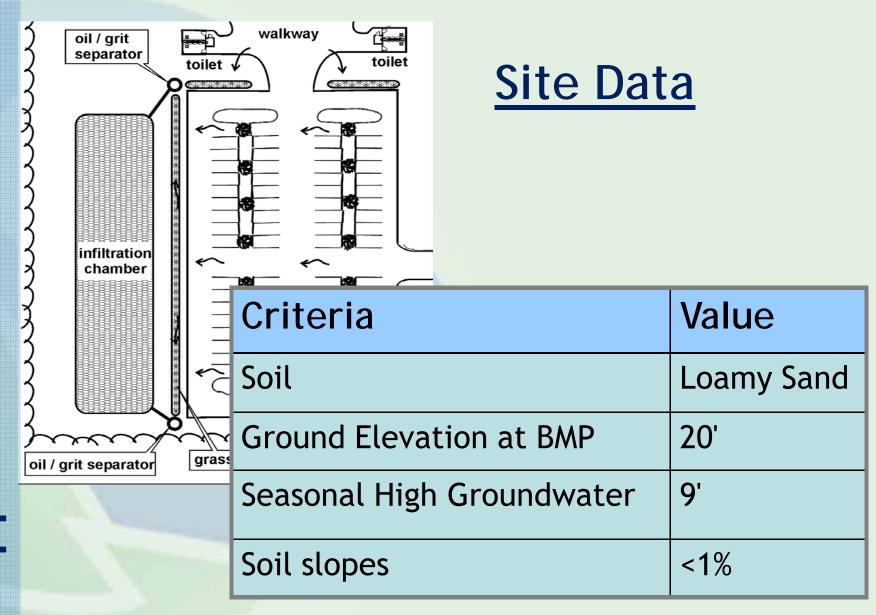
```
WQ_{v} = [(1") (I)] / 12
= [(1")(1.56 \text{ ac})] (1ft/12in)
= 0.13 \text{ ac-ft} = ~5,700 \text{ cf}
```



Min.
$$WQ_v = [(0.2")(DA)] / 12$$

= $[(0.2")(3.0 \text{ ac})] (1ft/12in)$
= $0.05 \text{ ac-ft} = ~2,200 \text{ cf}$

Cp_v and Q_p are <u>waived</u> since site discharges to coastal waters with tide effects
 Horsley Witten Group, Inc.





Horsley Witten Group, Inc.

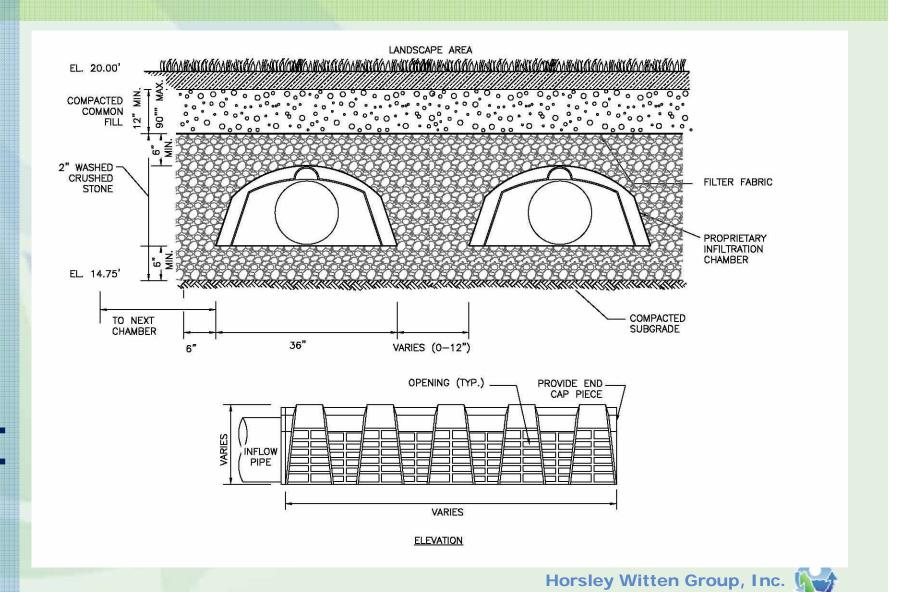
Design Criteria for Infiltration Chambers

Criteria	Status
Infiltration rate (f _c) greater than or equal to 0.5 inches/hour.	Design infiltration rate is 2.41 inches/hour. OK.
Soils have a clay content of less than 20% and a silt/clay content of less than 60%.	Loamy sand meets both criteria.
Infiltration cannot be located in fill soils.	Not fill soils. OK.
Hotspot runoff shall not be infiltrated.	Not a hotspot land use. OK.

Design Criteria, cont'd

Criteria	Status
The bottom of the infiltration facility must be separated by at least 3 feet vertically from the SHGT.	Elevation of seasonally high water table: 9' Elevation of BMP location: 20'. The difference is 11'. Thus, the facility can be up to 8' deep. OK.
Infiltration facilities must be located 50 feet horizontally from coastal features.	Chamber >50' from all coastal features. OK.
Maximum contributing area generally 5 acres or less.	Area draining to facility is < 5 acres. OK.
Setback 25 feet down- gradient from structures.	Chamber edge >25' from all structures. OK.

Cross-section Views of Chambers



Sizing Equation for Infiltration Chambers

Infiltration chambers can generally be sized by the equation below:

$$V = L * [(w * d * n) - (# *Ac * n) + (# * Ac) + (w * fc * T / 12)]$$

Where:

V = design volume (e.g., <u>WQv</u>) (cf)

L = Length of infiltration facility (ft)

w = Width of infiltration facility (ft)

H = Depth of infiltration facility (ft)

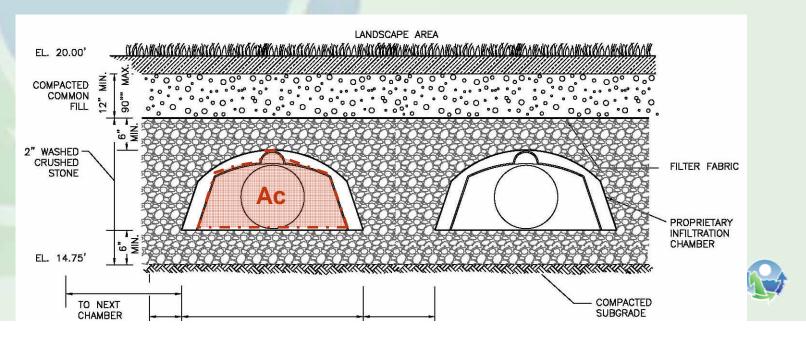
= Number of rows of chambers

A_c = Cross-sectional area of chamber

n = Porosity (assume 0.33)

 $f_c = \underline{Design}$ infiltration rate (in/hour)

T = Fill time in hrs



Solve for Length of Facility

Assume that:

n = 0.33

d = 4 feet

f = 2.41 inch/hour (*Table 5.2*)

T = 2 hours (use default value unless sitespecific data exists)

 $A_c = 3.5 \text{ sf } (supplied by manufacturer)$

= 15 ft / 3.25 ft (supplied by manuf.) =

4.6, only 4 rows can fit

Solve for Length given that we have 15' of width that we want to use at our site.



Therefore:

 $L = 5,700 \text{ ft}^3/[(15'*4'*0.33)-(4*3.5 \text{ ft}^2*0.33)+(4*3.5 \text{ ft}^2)+(15'*2.41 \text{ in/hr}^2 \text{ hr/12})]$

$$L = 5,700 \text{ ft}^3 / [(19.8 \text{ ft}^2) - (4.6 \text{ ft}^2) + (14 \text{ ft}^2) + (6.0 \text{ ft}^2)]$$

$$L = 162 ft$$



Final Sizing

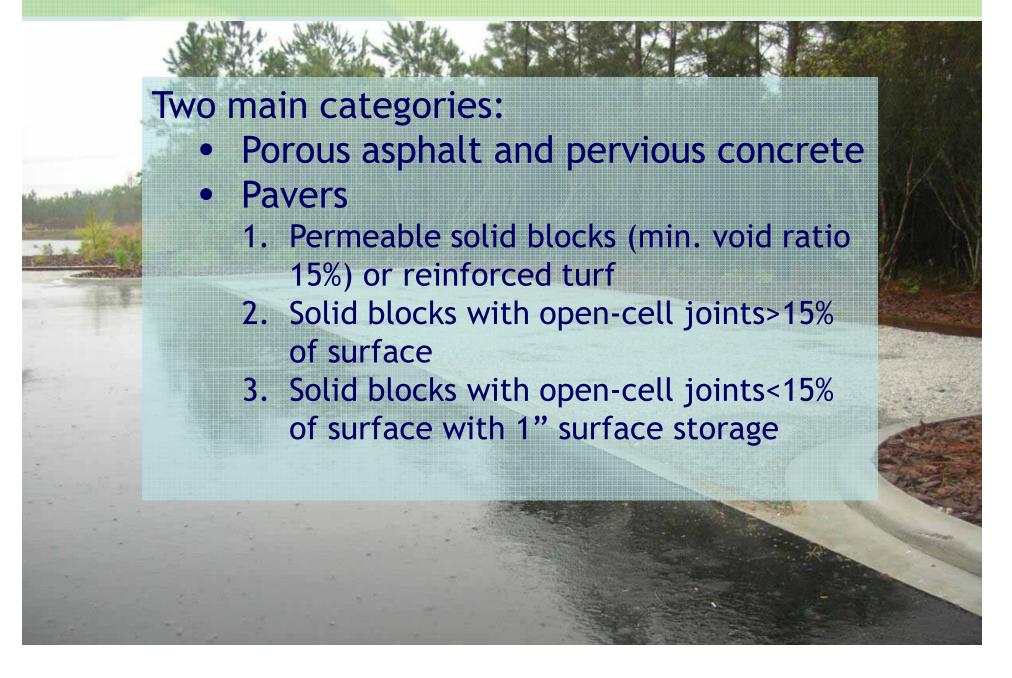
Add one foot to each end to give room for a stone buffer (more or less depending on manufacturer's specifications).



Facility dimensions will be 15' x 164'.

Check to ensure that there is sufficient room for the infiltration chamber facility alongside proposed parking lot. The proposed parking lot is 200 ft long, Ok.

Section 5.3: Permeable Paving



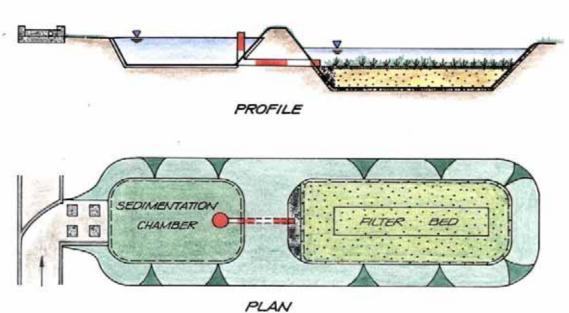
Permeable Pavements - Design Notes

- May be used as infiltration and/or detention system
- For infiltrating practices:
 - Field verification of soil permeability/texture essential
 - Bottom of facility cannot be located in fill* and must have 3' separation from gw and bedrock*
 - Size based on design infiltration rates (Table 5-3)
 - Cannot be used if contributing drainage is a LUHPPL
 - Must meet variety of setbacks* (Table 5-4)
- Frequent maintenance necessary to retain permeability (vacuum)
- Use on low traffic/speed areas with gentle slopes (<5%)
- Generally not designed to accept runoff from other areas
 - * Reduced requirements for resid. areas witten Group, Inc.

Section 5.5: Filtering Practices

- Sand/organic filters
- Bioretention areas/Tree filters







Filter Sizing Equation

$$A_f = (WQ_v) (d_f) / [(k) (h_f + d_f) (t_f)]$$

 A_f = surface area of filter bed (ft²)

d_f = filter bed depth (ft)

k = coef of permeability of filter media (ft/day)

h_f = average height of water above filter bed (ft)

 t_f = design filter bed drain time (days) (2 days is

recommended)





Sand/Organic Filter: Design Notes

- Pretreatment essential (25% WQv)
- Sized for temporarily holding at least 75% of WQv, including pretreatment
- Minimum depth of 18" (12" allowed in some instances)
- Use conservative permeability coef. (3.5 ft/day for sand, 2 ft/day for peat, and 8.7 ft/day for leaf compost)
- Need maintenance access to filter bed
- Useful to treat LUHPPL runoff



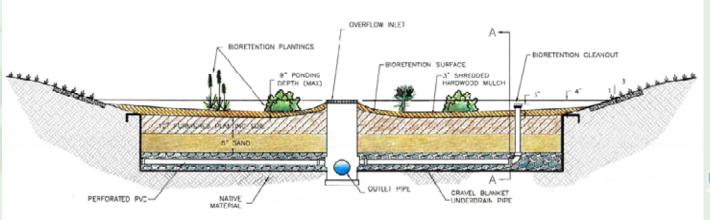
Bioretention: Design Notes

- Pretreatment essential (25% WQv)
- Sized for temporarily holding at least 75% of WQv, including pretreatment
- 6"-9" ponding above surface
- Typically, 2'-4' planting soil bed (12" allowed in some instances)
- Specific engineered soil media
- Use a conservative permeability coefficient
- Detailed landscape plan



Bio Planting Soil and Mulch

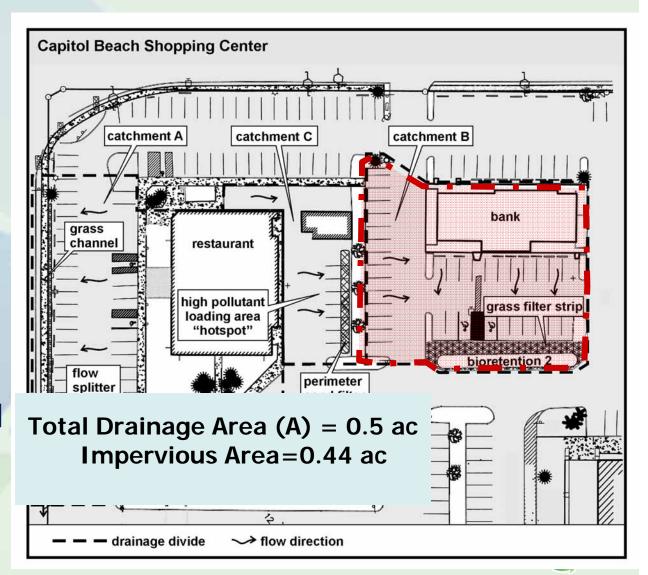
- Loamy Sand to a Sandy Loam
 - 85-88 % sand
 - 8-12 % silt
 - 0-2 % clay
 - 3 to 5 % organic matter
- Add well-aged, well-aerated leaf compost (20% by volume) for bios with shallow media depths (<2')
- Layer of well-aged, shredded hardwood mulch

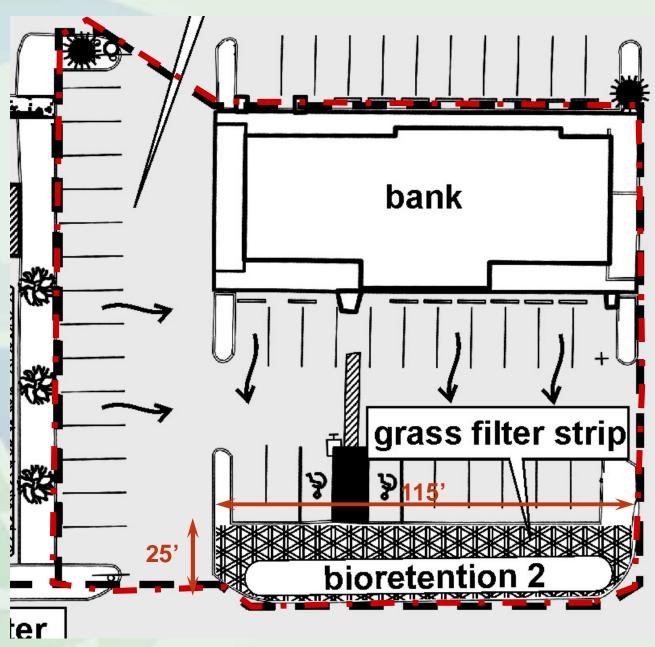




Bio - Sample Calculations

Capitol Beach Shopping Center is a hypothetical proposed development with a restaurant and bank. It is located in downtown Providence and discharges to the Providence River.





Site Specific Data:

- Site discharges to a large river (i.e., 4thorder or larger stream);
- On-site soils are "Paxton-Urban land Complex" (HSG C);
- Existing low point elevation at practice location is 10.0 ft; and
- Soil boring observations show seasonal high groundwater table at 2.0 ft.

Required Volume Calculations

Compute required Re_v based on C Soils and Sect. 3.3.2

```
Re_v = [(1") (F) (I)] / 12
= [(0.25")(0.44 ac)] (1ft/12in)
= 0.009 ac-ft = 390 cf
```

Compute WO_v

```
WQ_v = [(1") (I)] / 12
= [(1")(0.44 \text{ ac})] (1ft/12in)
= 0.037 \text{ ac-ft} = 1,610 \text{ cf}
```

- Cp_v and Q_p are waived since site discharges to a large river
- Bioretention will be designed without an impermeable liner to allow for infiltration.

Bioretention Sizing Equation

Use sizing equation and values provided in Section 5.5.4:

$$A_f = (WQ_V) (d_f) / [(k) (h_f + d_f) (t_f)]$$

 A_f = surface area of filter bed (ft²)

d_f = filter bed depth (ft) (2-4 ft, depending on site constraints)

k = coef of permeability of filter media (1 ft/day)

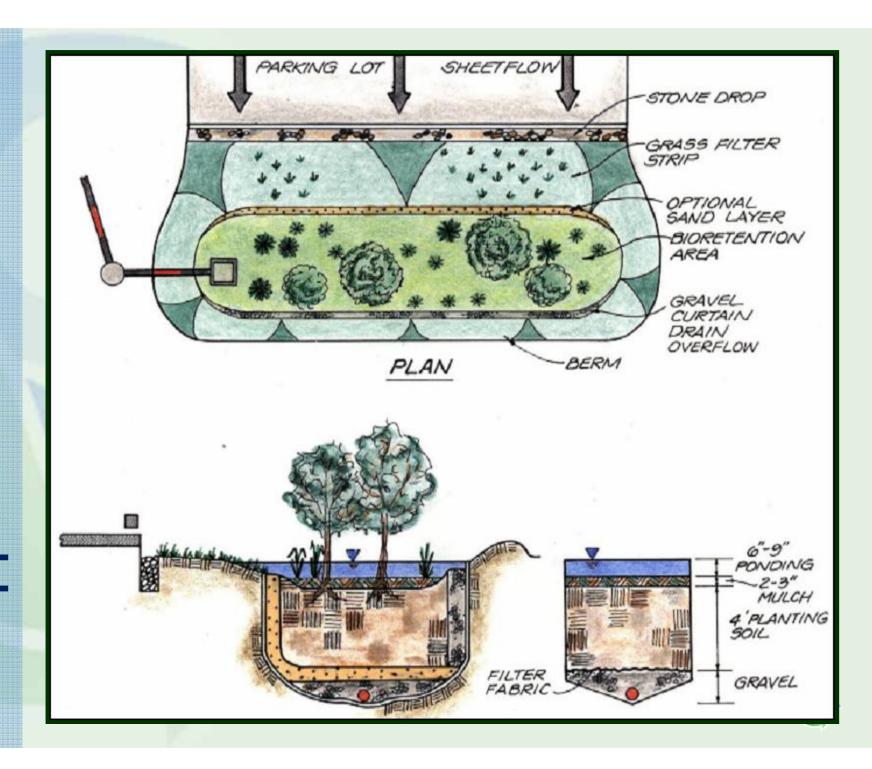
 $h_f = ave. ht of water above filter bed (ft) (1/2 of ponding depth)$

t_f = design filter bed drain time (days) (2 days recom.)

$$A_f = (1,610 \text{ ft}^3) (4') / [(1'/\text{day}) (0.25' + 4') (2 \text{ days})]$$

(With $d_f = 4'$, $k = 1.0'/\text{day}$, $h_f = 0.25'$, $t_f = 2 \text{ days}$)
 $A_f = 760 \text{ sq ft}$





Final Sizing

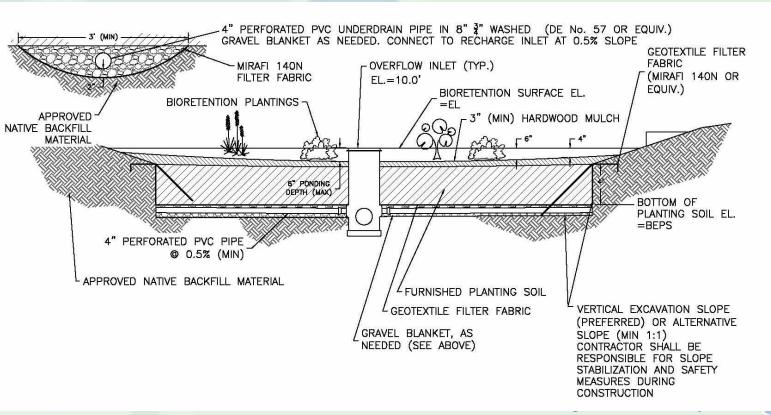
- Use width = 10'.
- Given a surface area requirement of 760 sq ft

Facility dimensions will be 10' x 76'.

 Check to ensure that there is sufficient room for the bioretention inside parking lot island. The proposed island is 115 ft long, Ok.

Cross-section of Bioretention

Set top of facility at 10', with the top of berm at 11'. The facility is 5' deep from rim to bottom of planting area, which will allow 3' of clearance above the SHGT.





Section 5.6: Green Roofs Design Notes

- Designed to manage WQv without bypass
- Safely convey runoff from larger storm events to a downstream drainage system
- No pretreatment required





Dry Swale: Design Notes

- Pretreatment: 10% WQv
- Use filter sizing equation
- 2 ft ≤ Bottom Width ≤ 8 ft



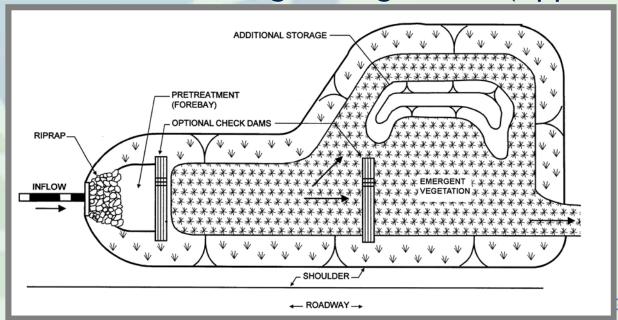
- Minimum 30" engineered bio soil (12" allowed in some instances)
- Maximum 12" deep average surface ponding depth
- Select the most appropriate native seed mix for expected swale conditions (Appendix B)
- Do not use on slopes greater than 4% w/o cells or checkdams
- Erosion control fabric for steeper grades
- May need some topsoil, fertilization, and irrigation to get grass established

 Horsley Witten Group, Inc.



Wet Swale: Design Notes

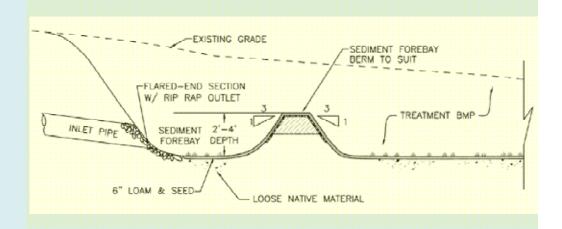
- Constructed in groundwater
- Pretreatment: 10% WQv
- Permanent pool may be included in WQv calculations
- 2 ft ≤ Bottom Width ≤ 8 ft
- Generally, <1% slope
- Planted with emergent vegetation (Appendix B)

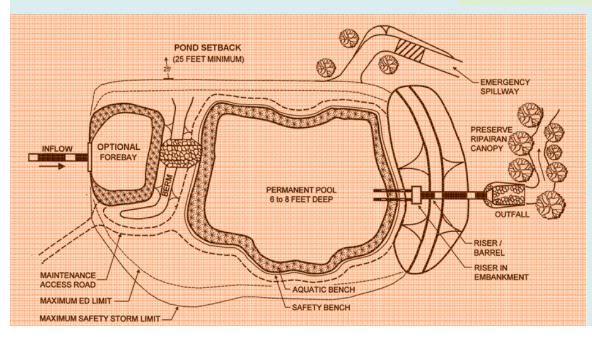




Practices Approved for Other Criteria

- Pretreatment Practices
 - Chapter 6
 - Grass Channel
 - Filter Strips
 - Sediment Forebay
 - Deep Sump Catch Basins
 - Proprietary Devices





- Storage Practices Chapter 7
 - Stormwater Basins
 - Underground Storage Devices
 - Infil. for Recharge/Storage

Pretreatment

Ch 3

Pretreatment Standards



Ch 5

- Approved BMPs for WQ Treatment
 - WVTS, infiltration, filters, green roofs, channels
 - Design requirements
 - Recommended design guidance
- Pretreatment Practices
 - Cannot be used alone to meet WQ
 - Grass channels, filter strips, sediment forebay, deep sump catch basins, proprietary devices

Horsley Witten Group, Inc.

Stormwater Standards

Standard 3

"...Pretreatment is required for water quality treatment practices where specified in the design guidelines within Chapter Five..."

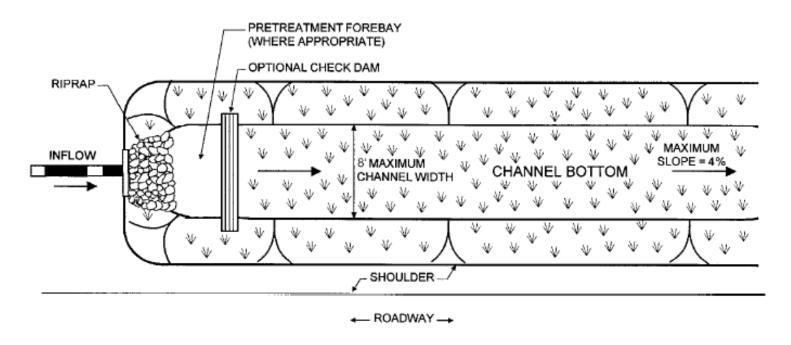
BMP Pretreatment Requirements

ВМР	Group	Required %WQ _v	Notes				
V	VVTS	10%	 Provided at each inlet, unless inlet provides <10% of inflow 				
Infiltration 2		25%	 Grass channel, filter strip, sediment forebay, proprietary device Deep sump catch basin <u>combined with</u> one of the following: Upper sand layer; or Washed pea gravel (1/8" to 3/8") Not required for permeable pavements (unless there is "run-on") or drywells 				
	tering actices	25%	 Deep sump catch basins may not be used as sole pretreatment. 				
	reen loofs	Not Applica	ble. No pretreatment required for direct rainfall.				
)pen annels	10%	forebays/checkdams at pipe inlets and/or driveway crossings.filter strip				

Grass Channels

Figure 6-1 Grass Channels

CHANNEL LENGTH IS DIRECTLY PROPORTIONAL TO ROADWAY LENGTH ----



* Gentle side slopes and dense vegetation can increase pretreatment



Filter Strip

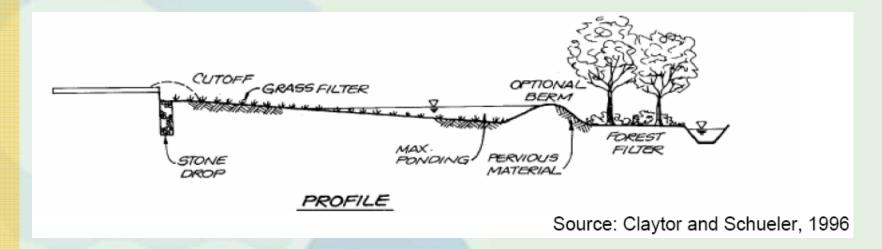
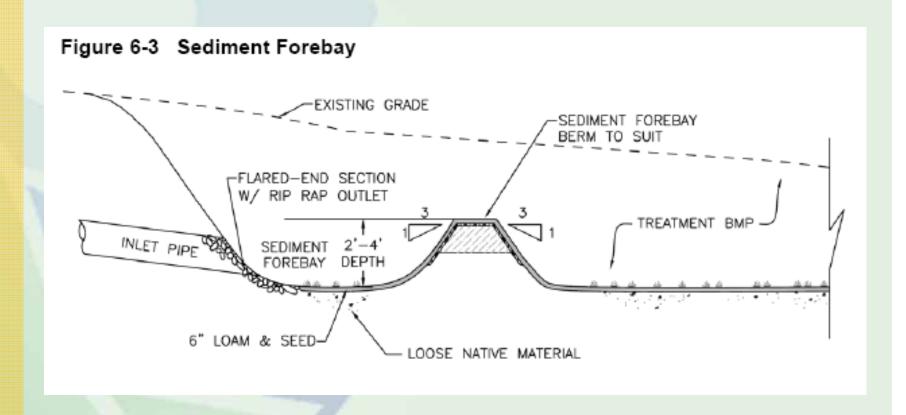


Table 6-1 Guidelines for Filter Strip Pretreatment Sizing

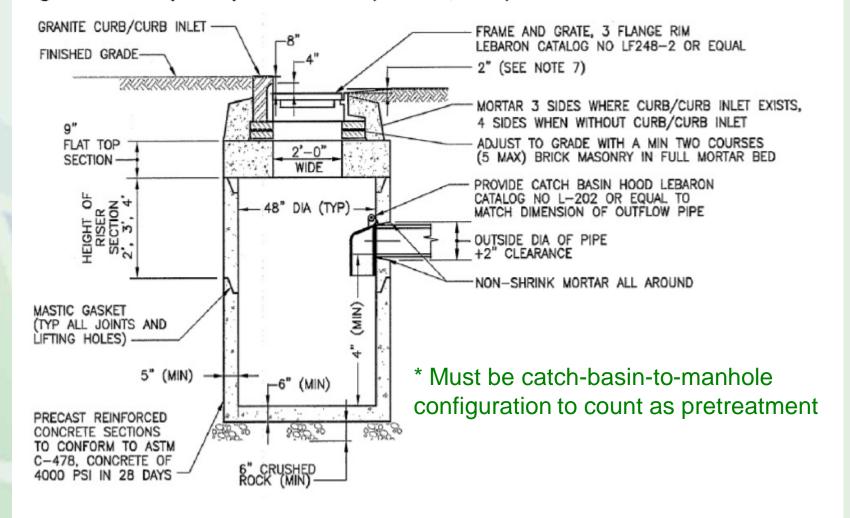
Parameter	Impervious Parking Lots				Residential Lawns			
Maximum Inflow Approach Length (ft)	35		75		75		150	
Filter Strip Slope (%)	<2	>2	<2	>2	<2	>2	<2	>2
Filter Strip Minimum Length (ft)	10	15	20	25	10	12	15	18

Sediment Forebay



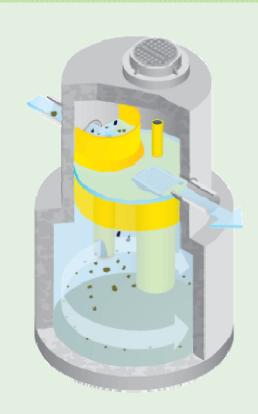
Deep Sump Catch Basin

Figure 6-4 Deep Sump Catch Basin (MADEP, 2008)



Proprietary Devices

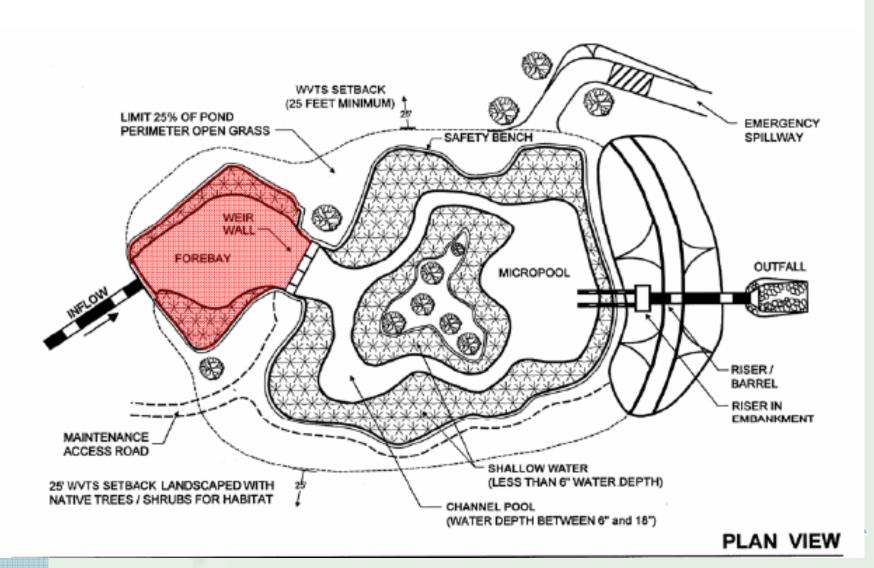
- Must have third-party verified
 25% TSS removal rate
- Flow-thru devices must be designed to handle entire WQ_f
- Must be designed as off-line (or have internal bypass) to allow large flows to bypass system
- Oil/grit separators great for LUHPPLs



Stormceptor® Extended oil storage (EOS) system

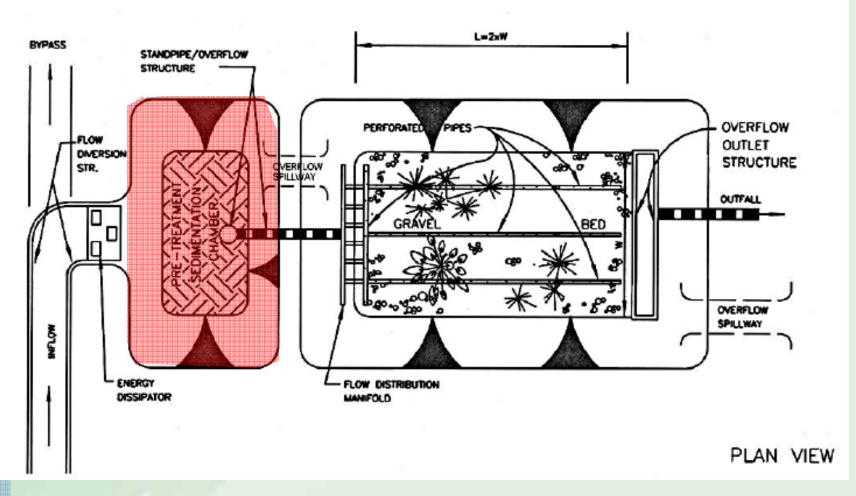
WVTS: Shallow WVTS

Figure 5-1 Shallow WVTS



WVTS: Gravel WVTS

Figure 5-2 Gravel WVTS – Alternative 1



Infiltration: Basins & Trenches

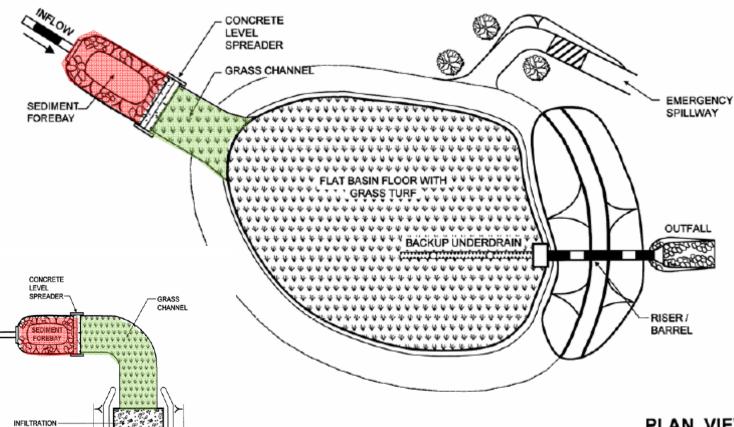
PLAN VIEW

ed WQ BMPs

PARKING LOT

(TO DETENTION FACILITY)

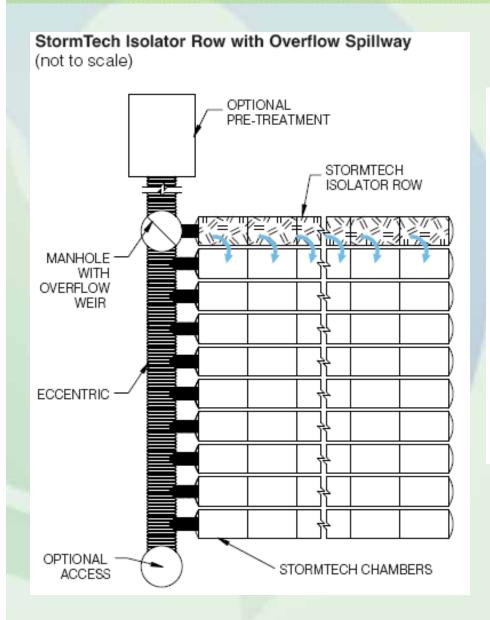
Figure 5-6 Infiltration Basin



PLAN VIEW

Horsley Witten Group, Inc.

Infiltration: Chambers







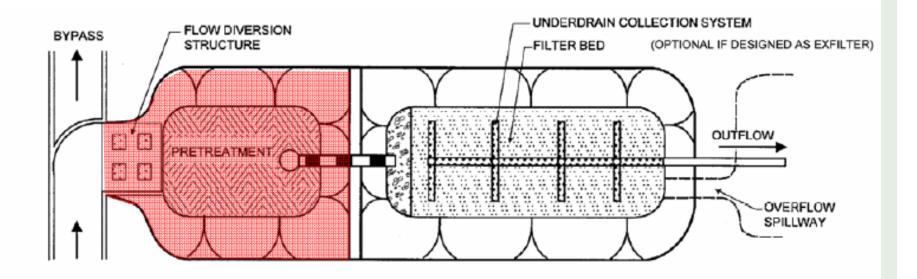
Isolator™ Row 0&M Manual StormTech® Chamber System for Stormwater Management



Filters: Sand & Organic Filter



Figure 5-12 Sand Filter







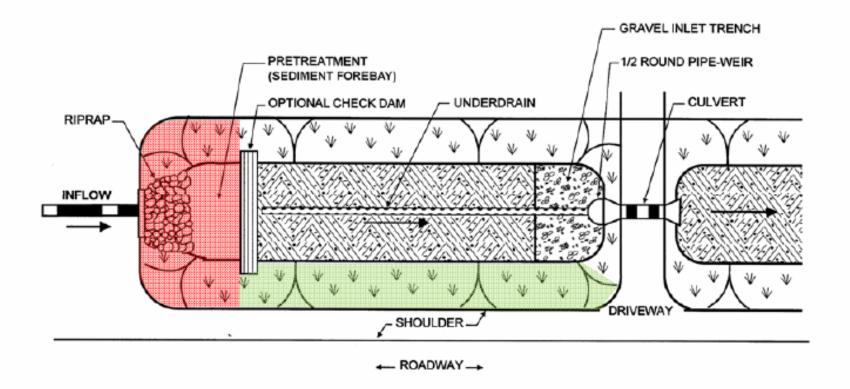
Filters: Bioretention

Figure 5-14 Bioretention PARKING LOT SHEET FLOW CURB STOPS-OPTIONAL STONE DIAPHRAGM OPTIONAL **GRASS FILTER** STRIP OPTIONAL SAND LAYER OPTIONAL **GRAVEL CURTAIN** OVERFLOW · DRAIN OVERFLOW "CATCH BASIN" BERM - UNDERDRAIN COLLECTION SYSTEM

(OPTIONAL IF DESIGNED AS EXFILTER)

Open Channels

Figure 5-17 Dry Swale





No pretreatment required

- Filters: Green roofs
- Infiltration: Permeable Pavers (unless there is "run-on"
- Infiltration: Dry Wells

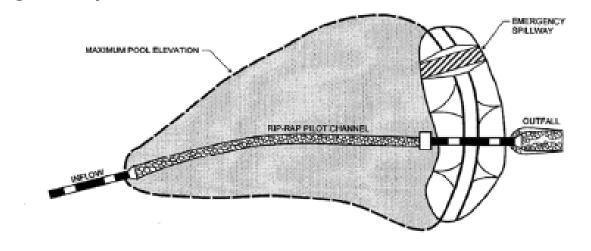
Quantity Standards



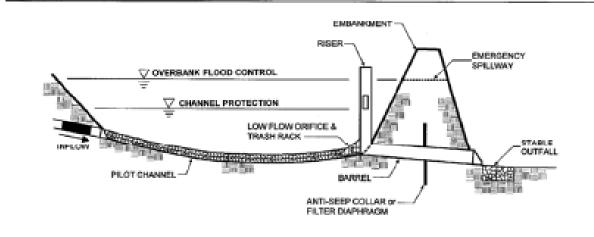
- Storage Practices
 - Cannot be used alone to meet WQ
 - Stormwater basins, underground storage facilities, and high-rate infiltration for recharge/storage only

Stormwater Basins

Figure 7-1 Dry Extended Detention Basin



PLAN VIEW



- Min. DA of25 acres forwet basins,unless in gw
- Permanent pool not included in storage calcs
- •Cold-water fishery restrictions

PROFILE



Enhanced Treatment

Using Basins for Additional Pollutant Loading Reduction

In order to use the removal rates for basins as listed in Appendix H.3 (Pollutant Loading Analyses) Table H-4, the following design criteria must be met.

Pretreatment

Required Elements

 Each basin shall have a sediment forebay or equivalent upstream pretreatment. The forebay shall be sized to contain 10% of the water quality volume (WQ_v) sized per Chapter 6. The forebay storage volume counts toward the total WQ_v requirement.

Treatment

Required Elements

- The minimum detention time for the WQ_v shall be 24 hours.
- Storage for the channel protection volume (CP_v) and the WQ_v shall be computed and routed separately (i.e., the WQ_v cannot be met simply by providing CP_v storage for the one-year storm).
- Provide water quality treatment storage to capture the computed WQ_v from the contributing drainage area through a combination of permanent pool and extended detention, as outlined in Table 7-1.

Table 7-1. Minimum Required Storage Volumes for Basins Used for Enhanced Pollutant Removal

Design Variation	%WQ _v				
Design variation	Permanent Pool	Extended Detention			
Dry Extended Detention Basin	20% min.	80% max.			
Wet Extended Detention Basin	50% min.	50% max.			

Design Guidance

Water quality storage can be provided in multiple cells. Performance is enhanced when
multiple treatment pathways are provided by using multiple cells, longer flowpaths, high
surface area to volume ratios, complex microtopography, and/or redundant treatment
methods (combinations of pool, extended detention, and shallow water).

Minimum Basin Geometry

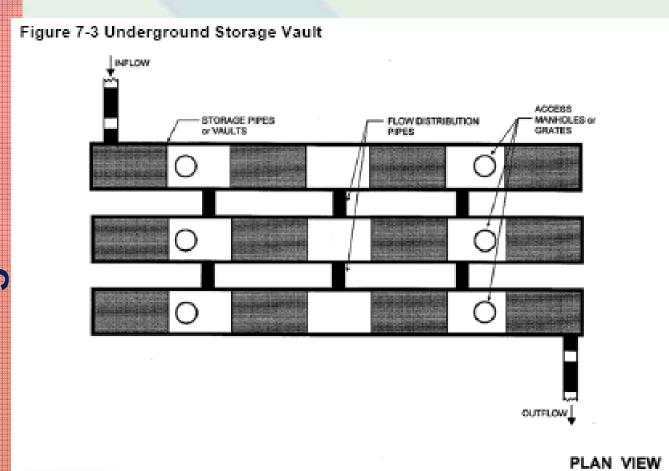
Required Elements

- The minimum length to width ratio for a basin shall be 1.5:1 (i.e., length relative to width).
- Provide a minimum Drainage Area: Surface Area Ratio of 75:1.
- Incorporate an aquatic bench that extends up to 15 feet inward from the normal edge of water, has an irregular configuration, and a maximum depth of 18 inches below the normal pool water surface elevation (see Figure 5-5).

Design Guidance

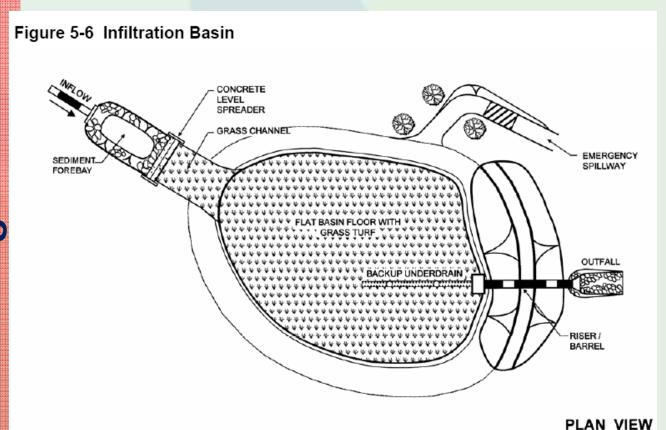
 To the greatest extent possible, maximize flow path through the system, and design basins with irregular shapes. To use basins for additional pollutant loading reduction, must design according to info on pg. 7-4

Underground Storage Devices



- Max. DA generally 25 acres
- •Sufficient access points shall be provided
- No coldwater fishery restrictions

Infiltration (Recharge/Storage Only)

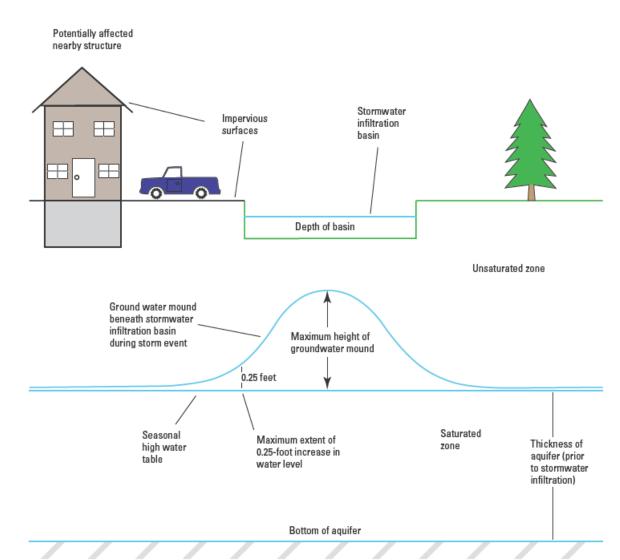


- •Sites with infiltration rates >8.3 in/hr
- Mounding analysis may be required
- May be constructed in suitable fill

Mounding Analysis

- When is it required?
 - Infiltration of stormwater (except for residential rooftops ≤ 1,000sf) AND
 - Separation to SHGT < 4' AND
 - On-line practice accepting runoff from the 10-year storm event and greater
- What does it tell us?
 - Feasibility of proposed BMP
 - Effect on nearby structures, OWTSs, etc.
- How is it done?
 - Hantush Method or equivalent

Simulation of Groundwater Mounding Beneath Hypothetical Stormwater Infiltration Basins



http://pubs.usgs.gov/sir/2010/5102

Scientific Investigations Report 2010–5102

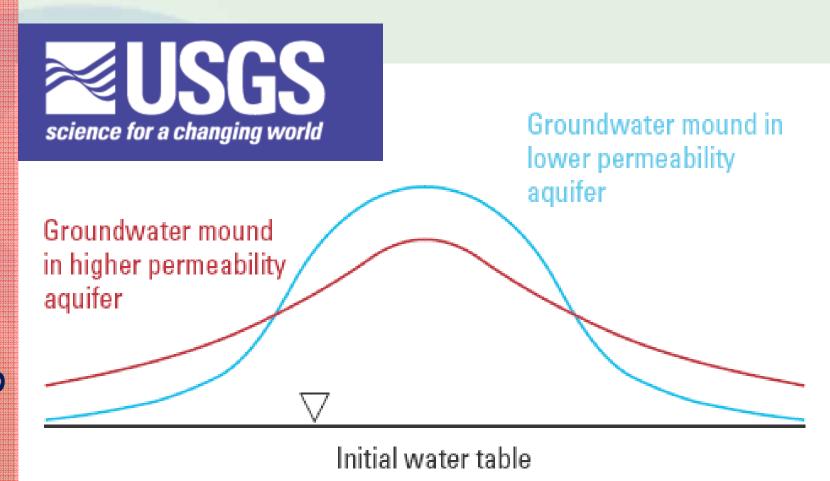


Figure 6. Schematic diagram showing relative shape of groundwater mounding in aquifers of higher and lower soil permeability.

Questions?

